## Feedback synthesis for motion of a material point with allowance for friction

Valery Korobov, Kharkiv, Ukraine Tetiana Revina, Kharkiv, Ukraine

Let us consider the feedback synthesis for motion of material point with allowance for friction:

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} x_2 \\ p(t, x_1, x_2)x_2 + u \end{pmatrix}.$$
 (1)

Here  $t \ge 0$ ,  $(x_1, x_2) \in \mathbb{R}^2$  is a state; u is a scalar control,  $|u| \le 1$ ;  $p(t, x_1, x_2)$  is unknown nonlinear viscous friction,  $p_1 \le p(t, x_1, x_2) \le p_2$ . The approach presented in the talk is based on the controllability function method proposed by V.I. Korobov in 1979. In [1] a control u(x) solving the feedback synthesis problem for system (1) without friction was given. It satisfies two conditions:

1)  $|u(x)| \leq 1$ ; 2) the trajectory x(t) starting from an initial point  $x(0) = x_0 \in \mathbb{R}^2$  of the closed system  $\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} x_2 \\ u(x) \end{pmatrix}$  ends at the origin at a finite time T > 0, and, in addition, the time T is equal to  $\Theta(x_0)$  for any  $x_0 \in \mathbb{R}^2$ .

The main goal of the research is to find friction limits such that a control steering the system without friction to the origin also steers the system with friction to the same target.

**Theorem 1.** Let  $a_1 < -4.5$ ,  $0 < \gamma_1 < 1$ ,  $\gamma_2 > 1$ , c > 0. The controllability function  $\Theta = \Theta(x_1, x_2)$  is defined for  $x \neq 0$  as a unique positive solution of the equation

$$\frac{(4+a_1)\Theta^4}{a_1(3+a_1)} - a_1x_1^2 + 4\Theta x_1x_2 + \Theta^2 x_2^2 = 0.$$
 (2)

$$\begin{aligned} \text{Let } Q &= \{ (x_1, x_2) \mid \Theta(x_1, x_2) \leq c \}, \\ p_1^0 &= \max\{ (1 - \gamma_1) \tilde{p}_1^0; (1 - \gamma_2) \tilde{p}_2^0 \}, \\ \tilde{p}_1^0 &= \frac{3 + a_1 - \sqrt{a_1(a_1 + 4)}}{c}, \end{aligned} \qquad \begin{aligned} u(x) &= \frac{a_1 x_1}{\Theta^2(x_1, x_2)} - \frac{3 x_1}{\Theta(x_1, x_2)}, \\ p_2^0 &= \min\{ (1 - \gamma_1) \tilde{p}_2^0; (1 - \gamma_2) \tilde{p}_1^0 \}, \\ \tilde{p}_1^0 &= \frac{3 + a_1 - \sqrt{a_1(a_1 + 4)}}{c}, \end{aligned} \qquad \begin{aligned} \tilde{p}_2^0 &= \frac{3 + a_1 + \sqrt{a_1(a_1 + 4)}}{c}. \end{aligned}$$

Then, for all  $p_1 \leq p(t, x_1, x_2) \leq p_2$  such that  $[p_1; p_2] \subset (p_1^0; p_2^0)$ , the trajectory of the closed system starting from an initial point  $x(0) = x_0 \in Q$  ends at the point x(T) = 0 at a finite time  $T = T(x_0, p_1, p_2)$  under the estimate  $\Theta(x_0)/\gamma_2 \leq T(x_0, p_1, p_2) \leq \Theta(x_0)/\gamma_1$ .

Furthermore we analyze the envelope for one-parametric family (2) at  $\Theta = 1$  for the system (1) with  $p(t, x_1, x_2) = 0$ . It is close to the curve that describes all points from which we may steer to the origin due to the Pontryagin maximum principle for the time t = 1.

 Choque Rivero A. E., Korobov V. I., Skoryk V. A. The controllability function as the time of motion 1.// Jour. Math. Phys. Anal. Geom. - 2004. - 11(2). - pp. 208 - 225.